

1.

$$(A) \quad \frac{R_4}{R_3} = \frac{R_6}{R_5}$$

$$V_o = \frac{R_4}{R_3} (V_{o2} - V_{o1}) \quad \text{by (9.52)}$$

$$\begin{cases} V_{o1} = (1 + \frac{R_2}{R_1}) V_{i1} - \frac{R_2}{R_1} V_{i2} \\ V_{o2} = (1 + \frac{R_2}{R_1}) V_{i2} - \frac{R_2}{R_1} V_{i1} \end{cases} \quad \text{by (9.65)}$$

$$\underline{V_o = \frac{R_4}{R_3} \left(1 + \frac{2R_2}{R_1}\right) (V_{i2} - V_{i1})} \quad \text{XX}$$

$$(b) \quad \frac{R_2}{R_1} = 1, \quad \frac{R_4}{R_3} = 10, \quad \frac{R_6}{R_5} = 12$$

$$\begin{aligned} V_o &= \left(1 + \frac{R_4}{R_3}\right) \left(\frac{R_6/R_5}{1 + R_6/R_5}\right) V_{o2} - \frac{R_4}{R_3} V_{o1} \\ &= 11 \times \frac{12}{1+12} V_{o2} - 10 V_{o1} \\ &= 10.1538 V_{o2} - 10 V_{o1} \end{aligned}$$

$$\begin{cases} V_{o1} = 2V_{i1} - V_{i2} \\ V_{o2} = 2V_{i2} - V_{i1} \end{cases}$$

$$\begin{aligned} V_o &= 10.1538(2V_{i2} - V_{i1}) - 10(2V_{i1} - V_{i2}) \\ &= 30.308V_{i2} - 30.1538V_{i1} \\ &= A_{cm} \left(\frac{V_{i1} + V_{i2}}{2}\right) + A_d (V_{i2} - V_{i1}) \\ &= A_{cm} V_{cm} + A_d V_{d} \end{aligned}$$

$$A_{cm} = 30.308 - 30.1538 = 0.1542$$

$$A_d = \frac{1}{2} (30.308 + 30.1538) = 30.2309$$

$$\text{CMRR (dB)} = 20 \log_{10} \left(\frac{30.2309}{0.1542}\right) = \underline{45.8473 \text{ dB}} \quad \text{XX}$$

2.

$$v_o = \left(\frac{333}{20}\right)(v_{o1} - v_{o2}) = 16.65(v_{o1} - v_{o2})$$

$$v_{o1} = -v_{BE1} = -V_T \ln\left(\frac{i_{C1}}{I_S}\right)$$

$$v_{o2} = -v_{BE2} = -V_T \ln\left(\frac{i_{C2}}{I_S}\right)$$

$$v_{o1} - v_{o2} = -V_T \ln\left(\frac{i_{C1}}{i_{C2}}\right) = V_T \ln\left(\frac{i_{C2}}{i_{C1}}\right)$$

$$i_{C2} = \frac{v_2}{R_2}, \quad i_{C1} = \frac{v_1}{R_1}$$

$$\text{So } v_{o1} - v_{o2} = V_T \ln\left(\frac{v_2}{R_2} \cdot \frac{R_1}{v_1}\right)$$

Then

$$v_o = (16.65)(0.026) \ln\left(\frac{v_2}{v_1} \cdot \frac{R_1}{R_2}\right)$$

$$v_o = 0.4329 \ln\left(\frac{v_2}{v_1} \cdot \frac{R_1}{R_2}\right)$$

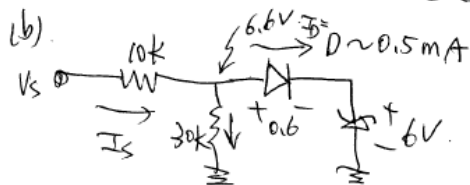
3.

(a). $v_Z = 6V$.

$$\frac{v_o}{v_Z} = \frac{10}{6} = 1 + \frac{R_2}{R_1}$$

$$\frac{R_2}{R_1} = 0.667 \quad *$$

$$1 \text{ mA} = \frac{10-6}{R_F} \Rightarrow R_F = 4 \text{ k}\Omega \quad *$$



① when $I_D = 0$

$$I_s = \frac{6.6}{30K} = 0.22 \text{ mA (min)} \quad *$$

② when $I_D = 0.5 \text{ mA}$

$$I_s = \frac{6.6}{30K} + 0.5 = 0.72 \text{ mA (max)} \quad *$$

4.
(a)

When no heat sink is used,

$$P_{D,\max} = \frac{T_{j,\max} - T_{\text{amb}}}{\theta_{\text{dev-case}} + \theta_{\text{case-amb}}} = \frac{150 - 30}{1.75 + 50} = 2.32 \text{ W}$$

When a heat sink is used,

$$\begin{aligned} P_{D,\max} &= \frac{T_{j,\max} - T_{\text{amb}}}{\theta_{\text{dev-case}} + \theta_{\text{case-snk}} + \theta_{\text{snk-amb}}} \\ &= \frac{150 - 30}{1.75 + 1 + 5} = 15.5 \text{ W} \end{aligned}$$

- (b)

$$T_{\text{snk}} - T_{\text{amb}} = P_D \cdot \theta_{\text{snk-amb}}$$

or

$$T_{\text{snk}} = 30 + (15.5)(5) \Rightarrow T_{\text{snk}} = 107.5 \text{ }^\circ\text{C}$$

The case temperature is found from

$$T_{\text{case}} - T_{\text{amb}} = P_D \cdot (\theta_{\text{case-snk}} + \theta_{\text{snk-case}})$$

or

$$T_{\text{case}} = 30 + (15.5)(1 + 5) \Rightarrow T = 123 \text{ }^\circ\text{C}$$

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- 5.

$$V_{CEQ} = 6 = V_{CC} - I_{CQ}R_L = 12 - I_{CQ}(1) \Rightarrow I_{CQ} = 6 \text{ mA}$$

$$\overline{P}_L = \frac{1}{2} \cdot \frac{V_P^2}{R_L} = \frac{1}{2} \frac{(4.5)^2}{1} = 10.1 \text{ mW}$$

$$\eta = \frac{10.1}{I_{CQ}V_{CC}} \times 100\% = \frac{10.1}{(6)(12)} \times 100\% = 14.1\%$$